

Focal L-band Array for the GBT (FLAG): Instrumentation Upgrades and Initial Commissioning results

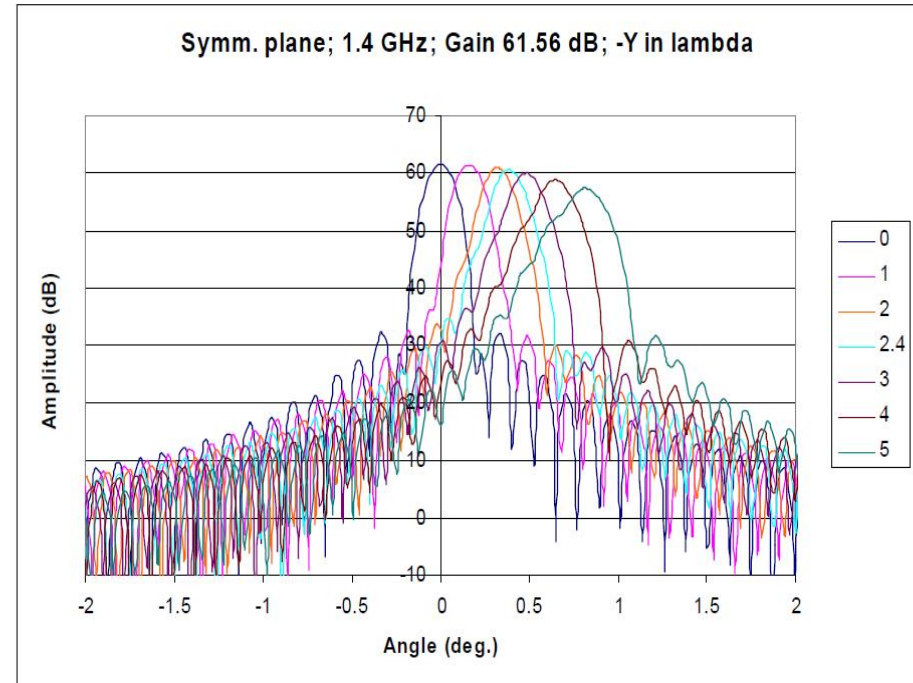
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W. Groves, T. Chamberlin, R. Prestage, J. Ray,
R. Simon, V. van Tonder, S. White
NRAO, Charlottesville and Green Bank

K. F. Warnick, B. D. Jeffs
Brigham Young University, Utah

- Motivation to build FLAG, NRAO FLAG history
- Summary : 2015 Cyro-PAF system, GBT commissioning, NRAO PAF model development
- 2016: New Instrumentation development and Initial measurments on the GBT
- Future work

Field of View of GBT at L-band



Srikanth (2006)

Figure 2. GBT beams at 1.4 GHz for offsets (λ) in symmetric plane towards the feed arm

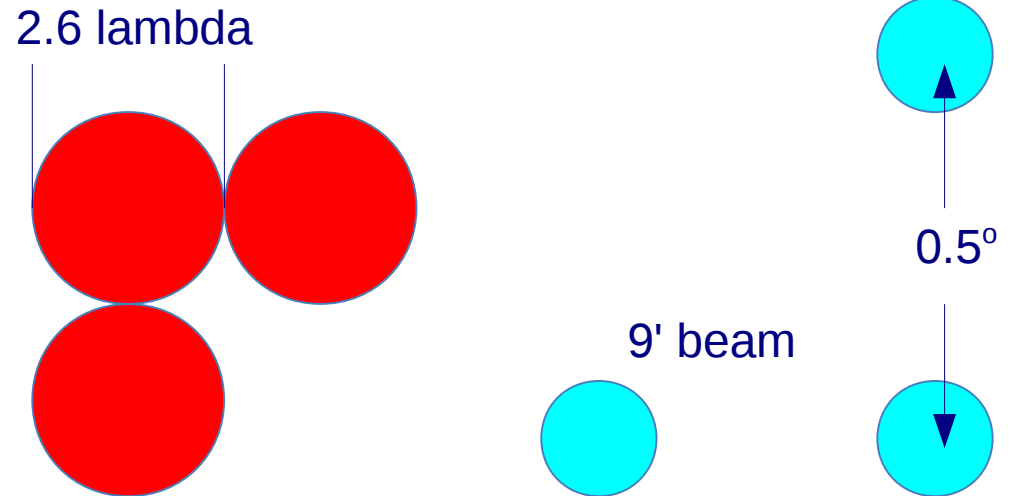
Green Bank Telescope (GBT); 100 m dia; ang resolution at 1.4 GHz is 9'

FOV – angular region where the beam aberration is within a specified tolerance. (for GBT $\sim 1^\circ \times 1^\circ$ for 1 dB loss in gain)

Focal Plane Array vs Phased Array Feed

An example 1.4 GHz prime-focus feed array for GBT

Beam $\sim 9'$
Feed size ~ 2.6 lambda ~ 55 cm

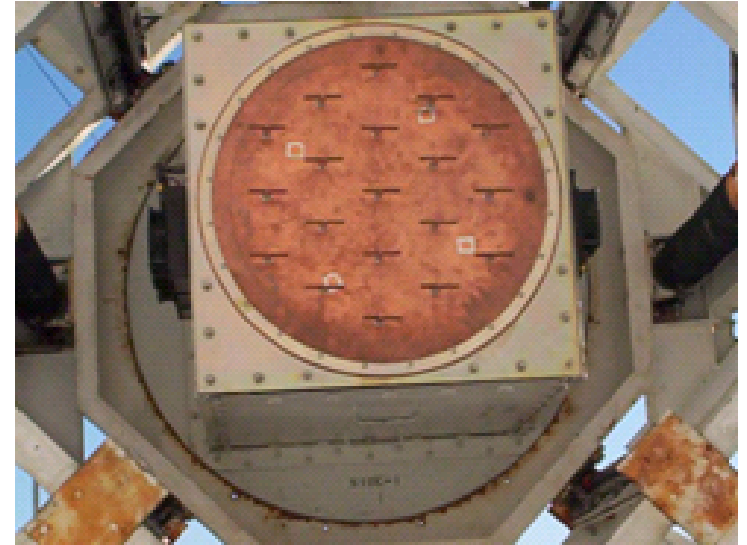


- Feed designed to maximize telescope gain and minimize spillover
- FPA with L-band feed – 9' beam separated by 0.5°
- Sky sampling not good for imaging
- Solution to overcome these difficulties – PAF

NRAO PAF History



Sinuuous element
140 ft 1996



Thin Dipoles
20-m 2007



• 19 dual polarized elements

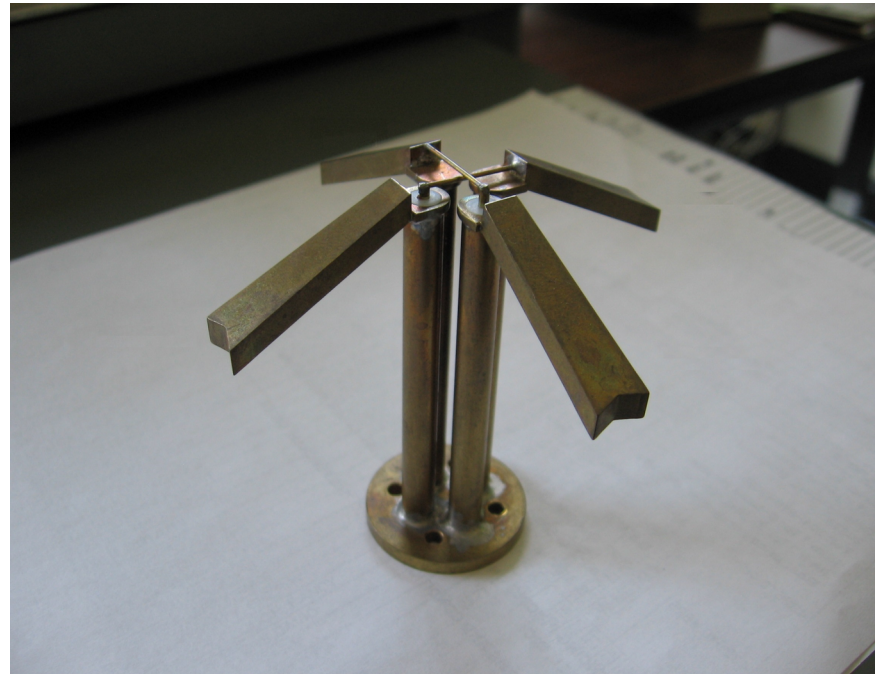
Thick, impedance-optimized dipoles, 20-meter, 2010



Cryo-PAF used for 2015 commissioning



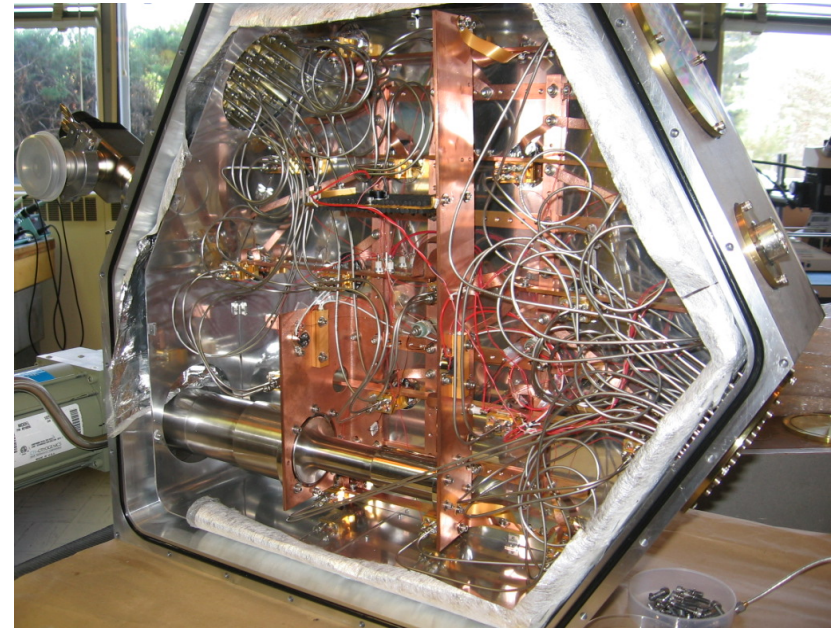
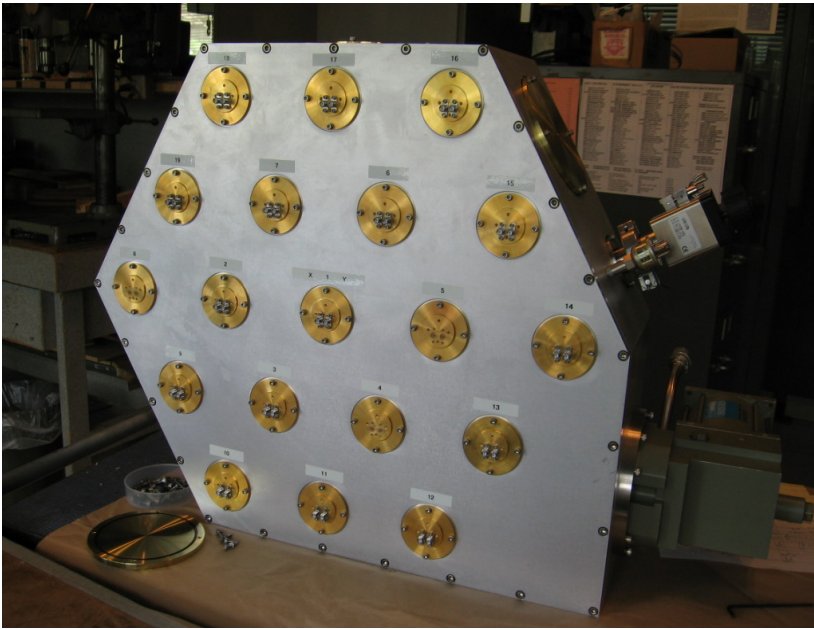
19 element dual polarized Kite Array



Kite Dipole

Weinreb SiGe LNAs

2015 Cryostat for 19 element PAF



Cooled LNA receiver-Dewar;

2-stage GM cooler; Cooled to 15 K

Developed by Roger Norrod at NRAO.

2015 PAF system and Signal Processing



Kite
Array

Amplifiers
Analog Fiber
transmitters

Analog Fiber
receivers
Downconverters

500 KHz BW
12 bit ADC and
voltage recorder

- Receiver connected to backend through analog fiber links
- Digitize (12 bits) and record voltage
- Process data off-line

$$v_{out} = \mathbf{w}^T \mathbf{V}; \quad \mathbf{w} \text{ is beamformer weights}$$

$$\langle v_{out} v_{out}^* \rangle = \mathbf{w}^H \mathbf{R} \mathbf{w}$$

$$\mathbf{R} = \langle \mathbf{V} \mathbf{V}^H \rangle; \quad \text{Correlation of output voltages}$$

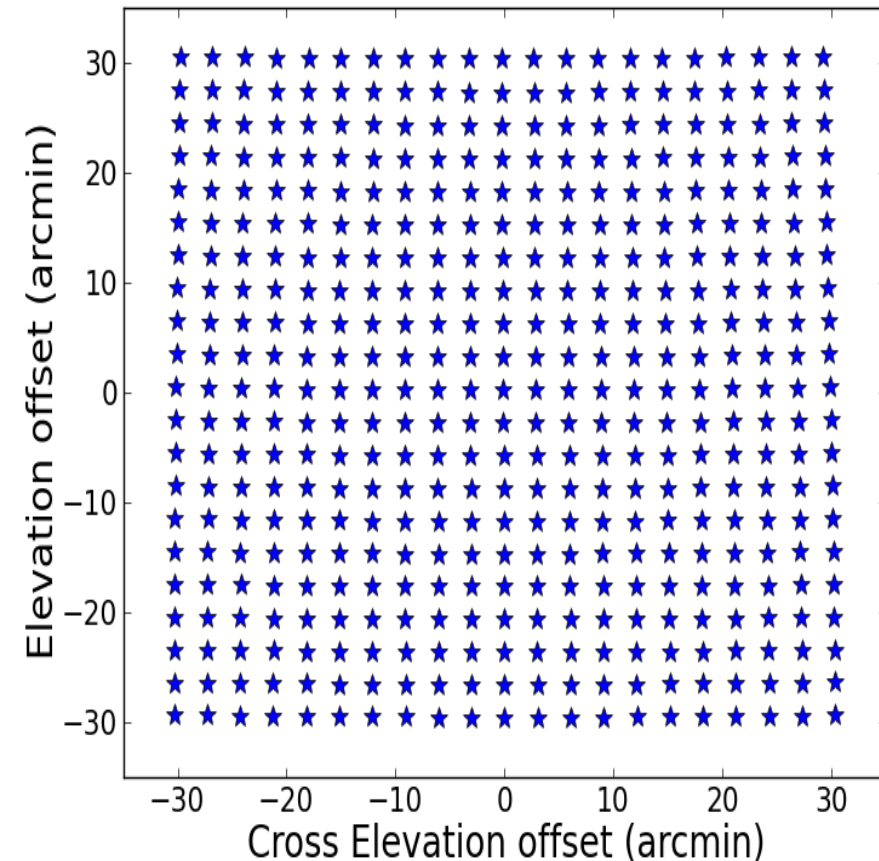
2015: Observations with the GBT

Grid Obs :

- GBT beam at 1.7 GHz ~ 7', Grid pos ~ 3'
- Observed radio galaxy Virgo A
- Freq of obs 1700 MHz

Freq Scan Obs :

- Made On-Off observations on Calibrators
- Freq scanned from 1250 to 1800 MHz in steps of 50 MHz



Max SNR Beamforming

- Using On-Off data on calibrator

\mathbf{R}_{on} , \mathbf{R}_{off} – On & Off correlation matrix, \mathbf{w} is beamformer weights

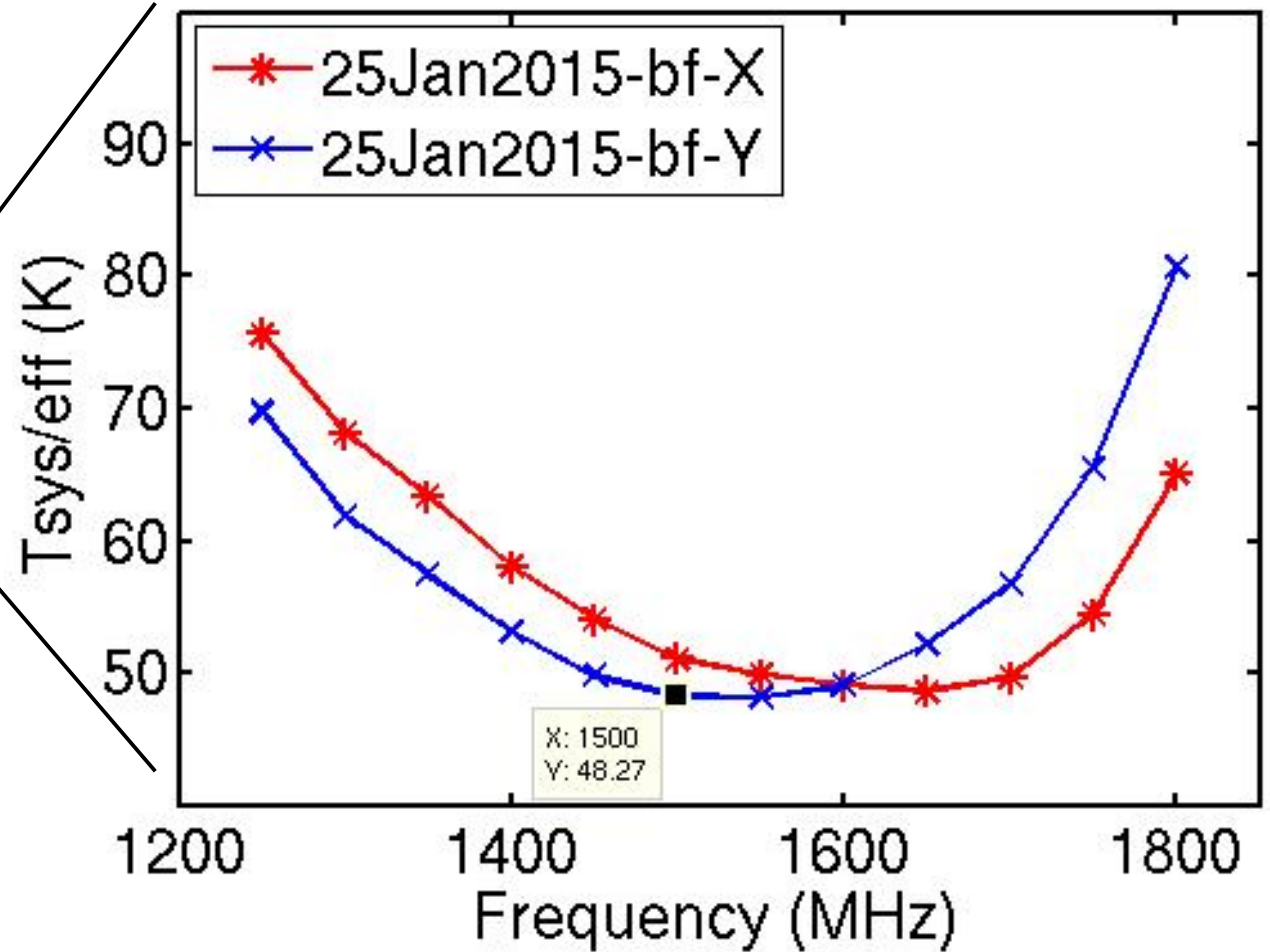
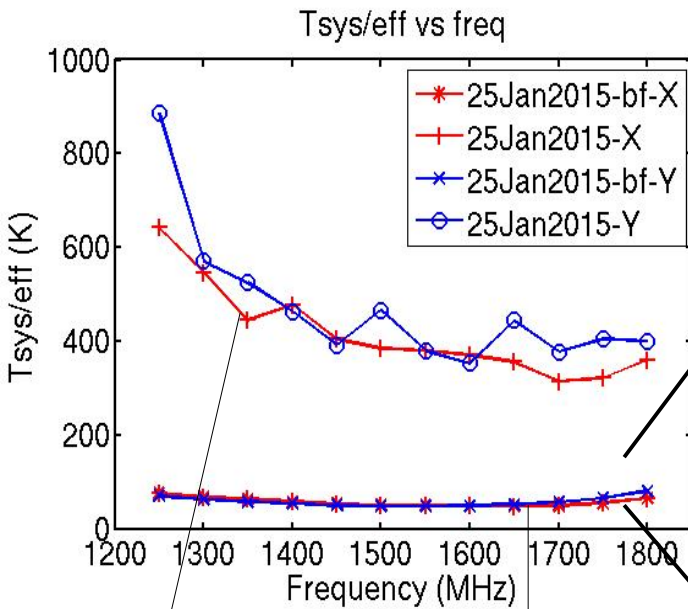
- $$\text{SNR} = \frac{\mathbf{w}^H (\mathbf{R}_{\text{on}} - \mathbf{R}_{\text{off}}) \mathbf{w}}{\mathbf{w}^H \mathbf{R}_{\text{off}} \mathbf{w}}$$

- Max (generalized) Rayleigh quotient gives the best SNR
- Eigenvector of the max Rayleigh quotient gives \mathbf{w} for best SNR

- Performance – T_{sys} / η ; $\text{SNR} = \frac{0.5 S A \eta}{kT_{\text{sys}}}$

2015: Boresight beam T_{sys}/η on Virgo A

$T_{\text{sys}}/\text{eff}$ vs freq for bore sight beam

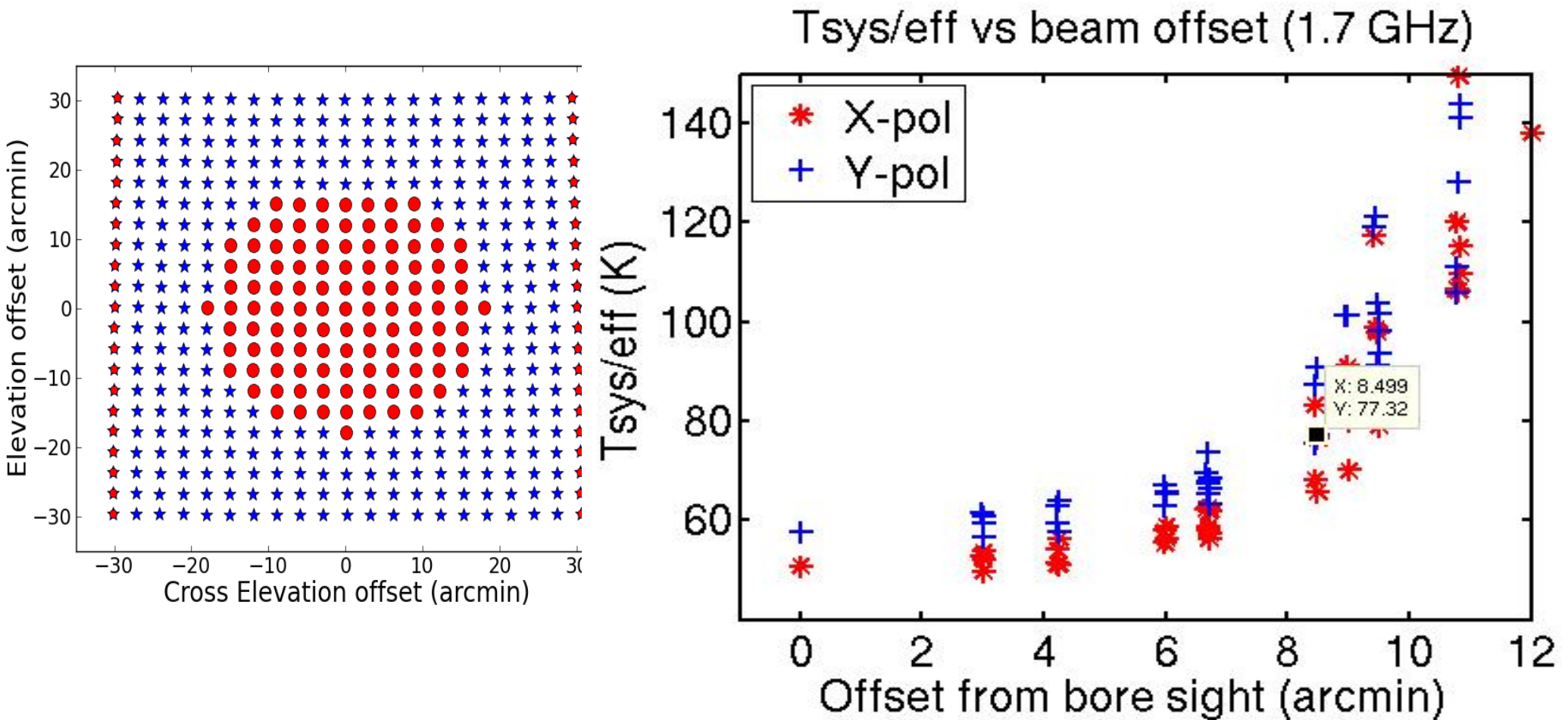


Formed beam

Central Dipole

$T_{\text{sys}}/\eta = 48.2 \text{ K @ } 1550 \text{ MHz}$

2015: Off-boresight T_{sys}/η



• $T_{\text{sys}}/\eta = 63 \text{ K @ } 7'.2 \text{ (FWHM) @ } 1.7 \text{ GHz}$

• Survey speed compared to GBT L-band feed : PAF is 20% better

NRAO PAF model

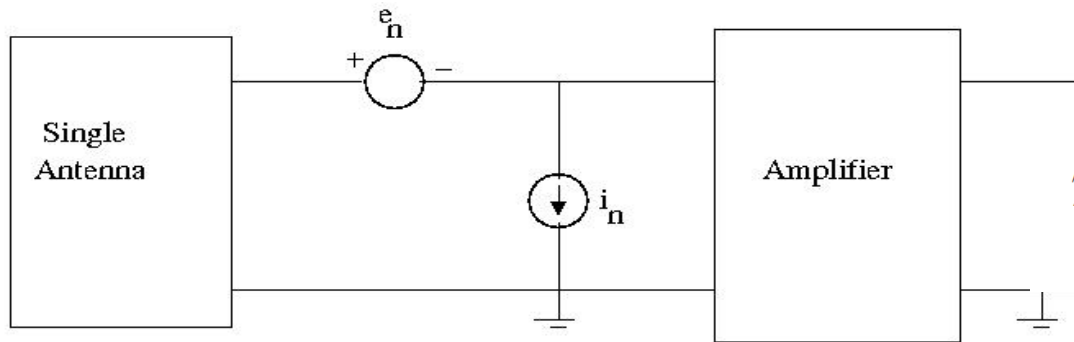
Question: For a PAF installed on a telescope what is the best (spectral) T_{sys}/η that can be obtained when observing a source at some angle (θ_s, φ_s) from the boresight direction ?

Answer:

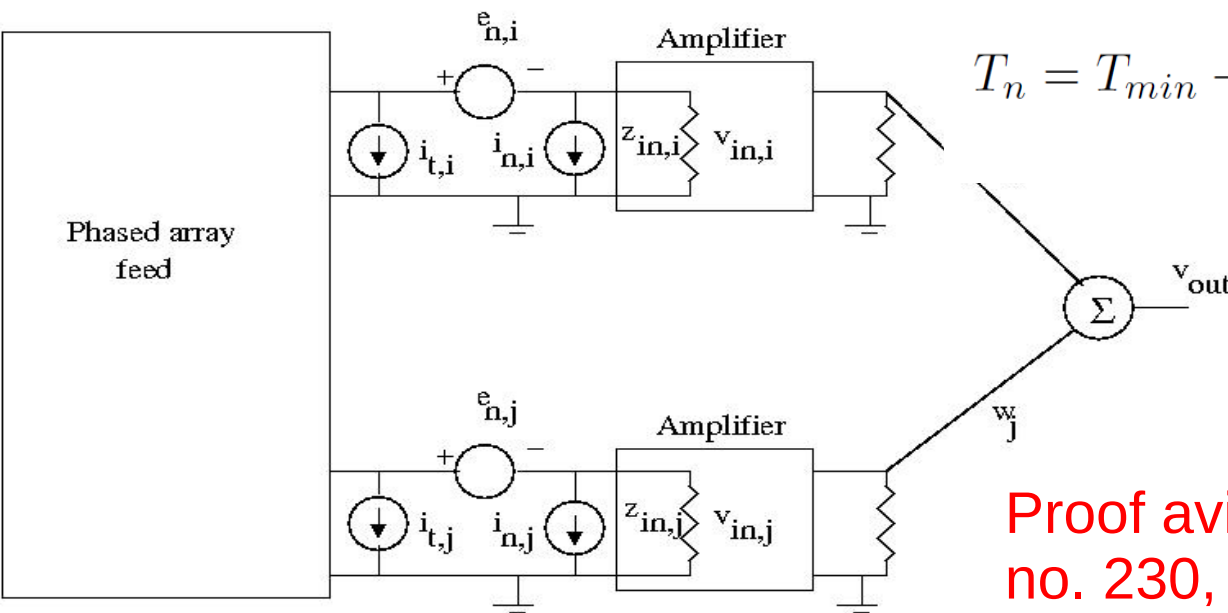
Theorem: Given (spectral) \mathbf{Z} , $\mathbf{E}_i(\theta, \varphi)$, amplifier noise parameters (R_n, g_n, ρ) and given the telescope geometry and source position, one can construct a characteristic matrix \mathbf{M} for the system. Then, the best signal-to-noise ratio on the source is the maximum eigenvalue, e_{max} , of \mathbf{M} .

Proof available in NRAO EDIR 2016, no. 230, Roshi & Fisher

PAF model: Receiver Temperature



$$T_n = T_{min} + NT_0 \frac{(Z_s - Z_{opt})(Z_s - Z_{opt})^*}{\text{Re}\{Z_s\} \text{Re}\{Z_{opt}\}}$$

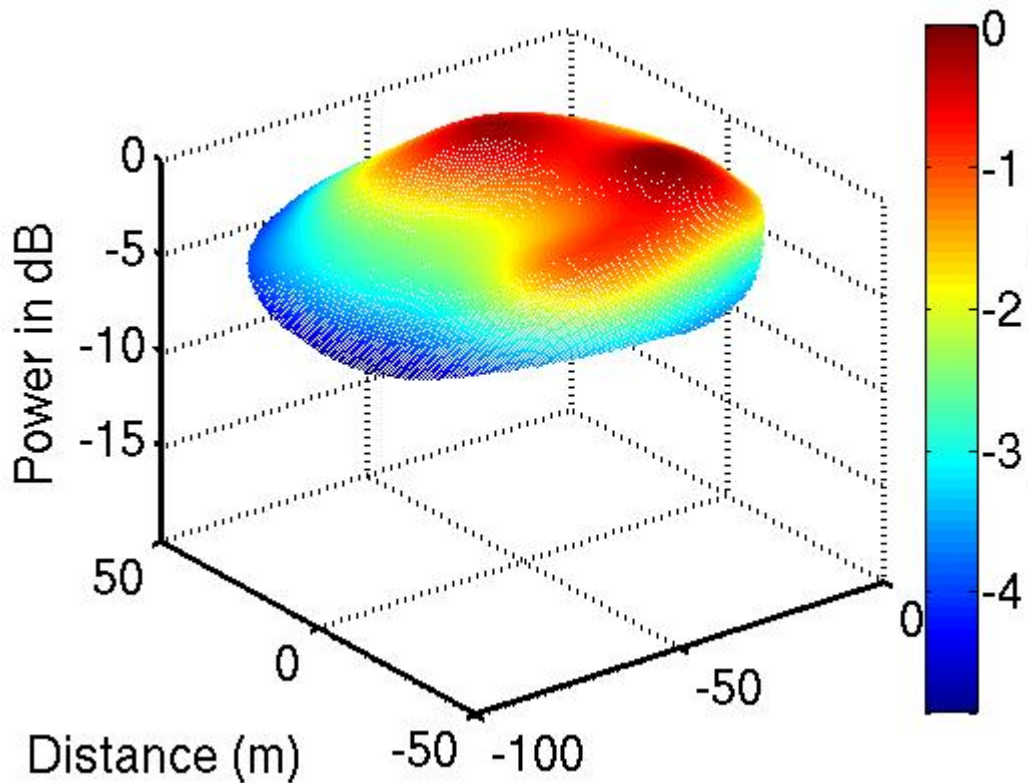


$$T_n = T_{min} + NT_0 \frac{\mathbf{w}_1^H (\mathbf{Z} - Z_{opt} \mathbf{I})(\mathbf{Z} - Z_{opt} \mathbf{I})^H \mathbf{w}_1}{\text{Re}\{Z_{opt}\} \frac{1}{2} \mathbf{w}_1^H (\mathbf{Z} + \mathbf{Z}^H) \mathbf{w}_1}$$

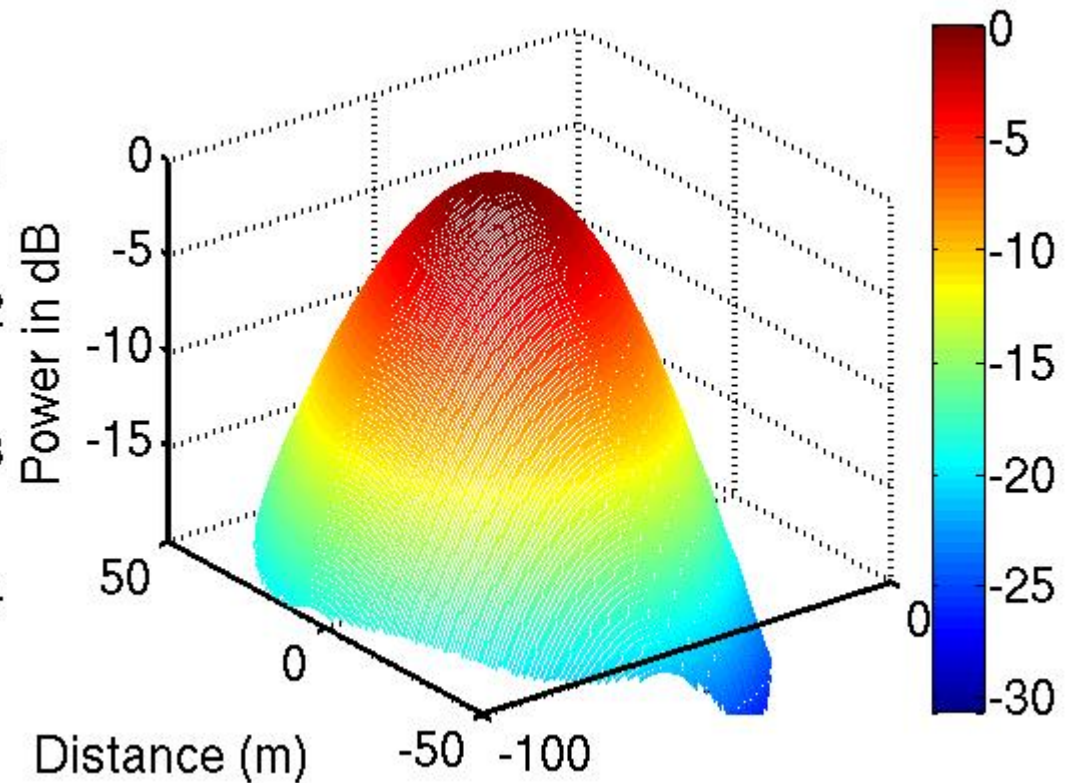
(for identical amplifiers)

Proof available in NRAO EDIR 2016, no. 230, Roshi & Fisher

PAF model: GBT Aperture Field Pattern



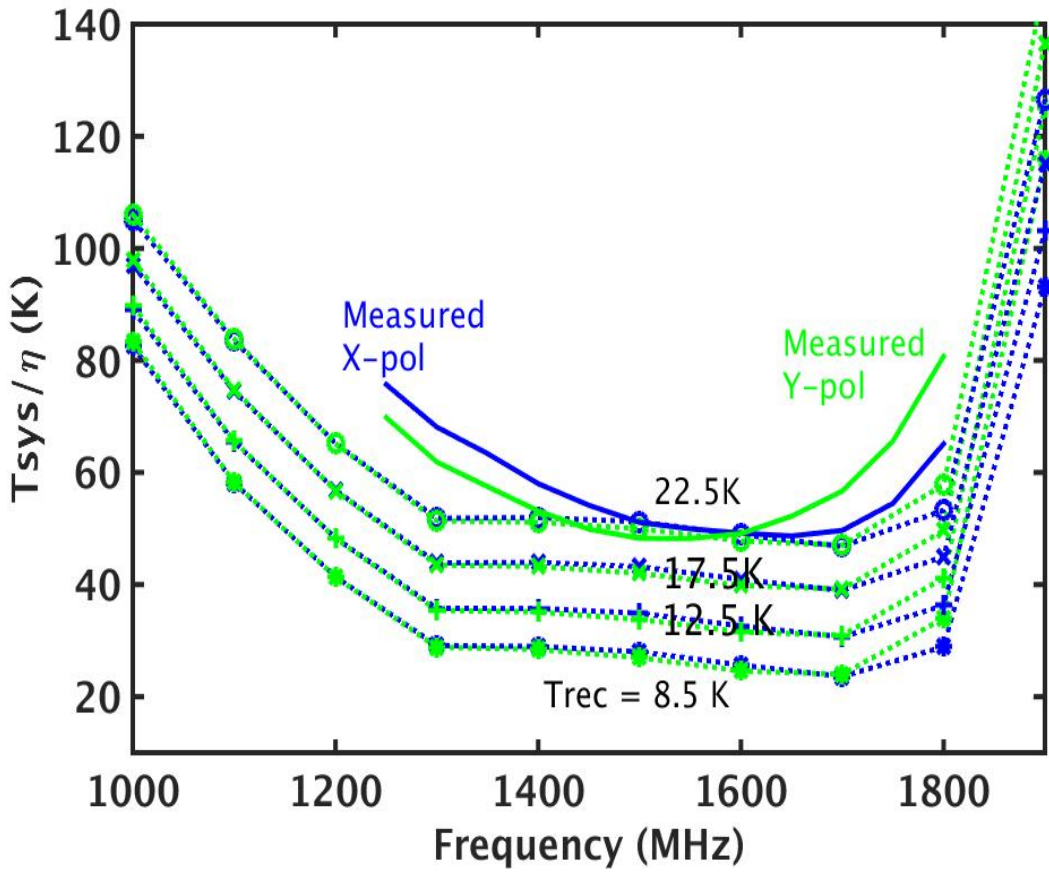
Dipole 1, X-pol



Max SNR wt-ed X-pol field

NRAO PAF model vs 2015 obs

Boresight beam



Thermal transition	4 K
Replacement transistor	5 K
Excess needed	5 K

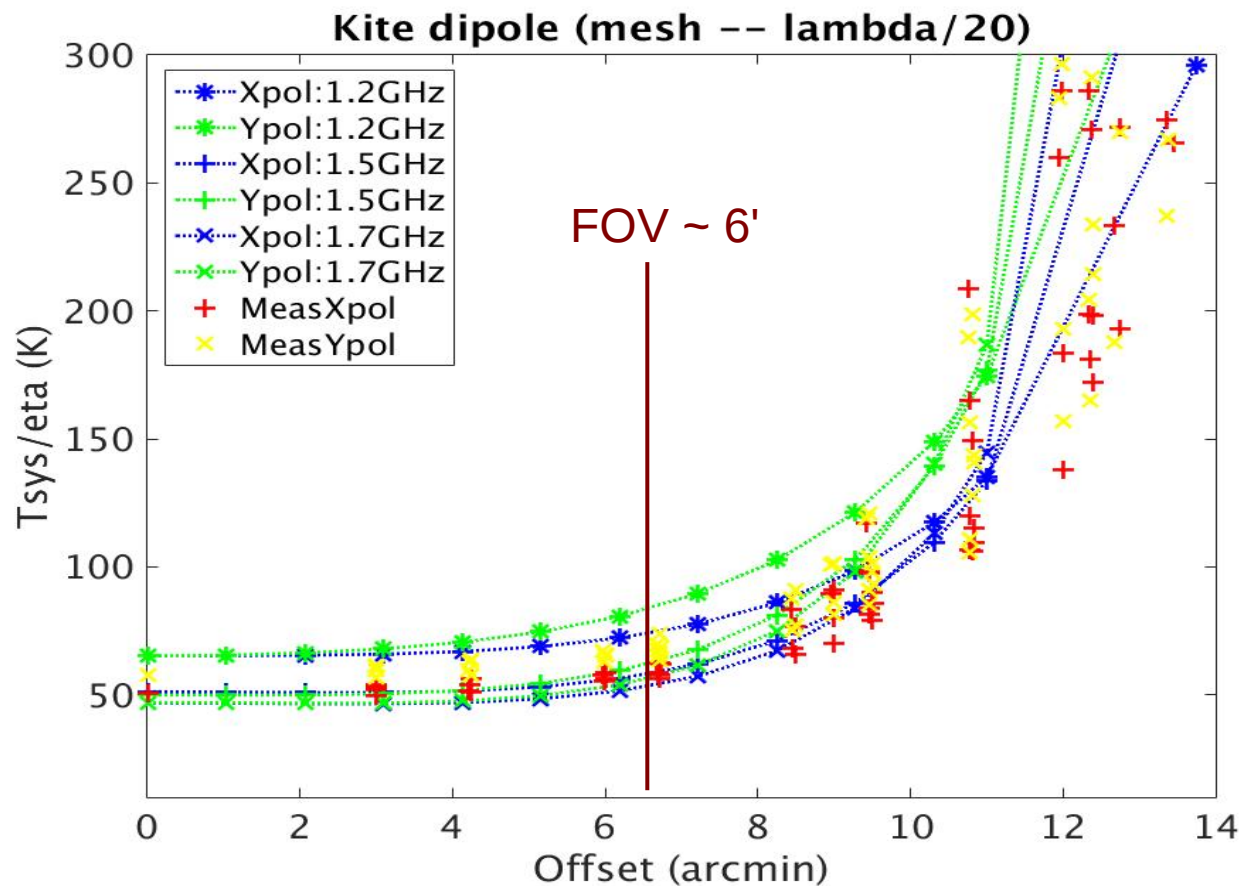
Antenna Loss	?
Excess noise in Down converter	4 K

$T_{rec} \sim 22$ K for model to match measurement

T_{rec} is 5 K above what can be accounted for

NRAO PAF model vs 2015 obs

Off-boresight beam

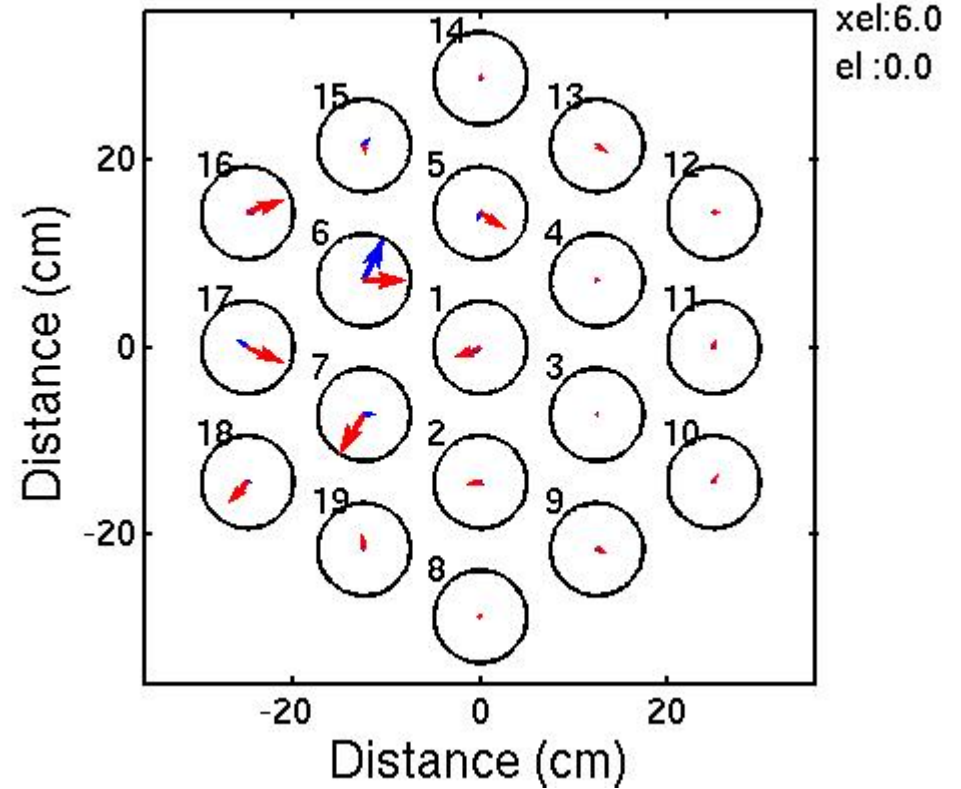
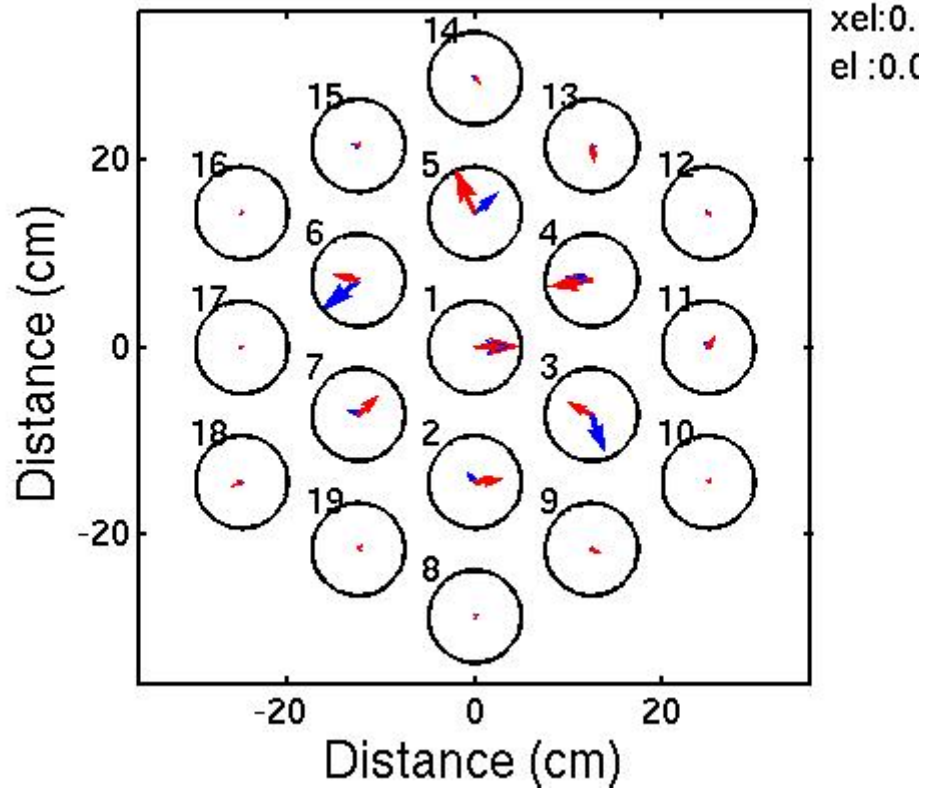


Model results match well with measurements for $T_{rec} \sim 22$ K

Spillover efficiency – 97 % for $T_{rec} \sim 22$ K

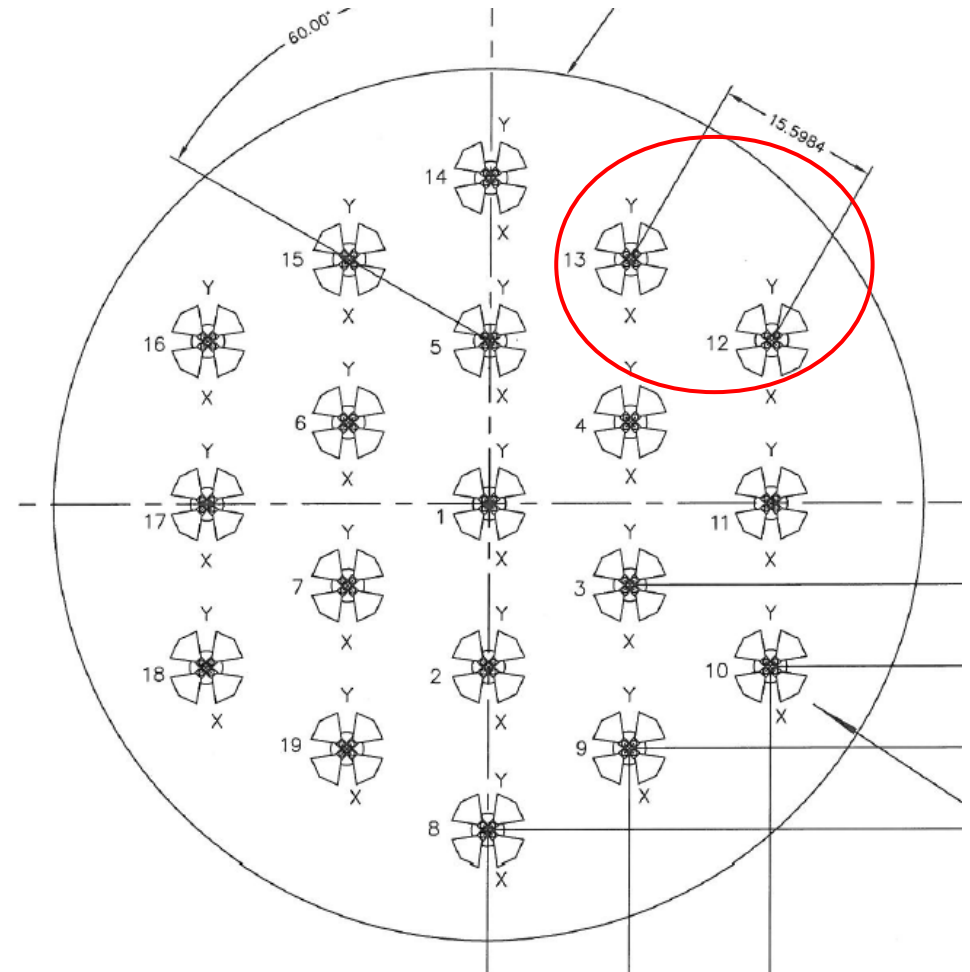
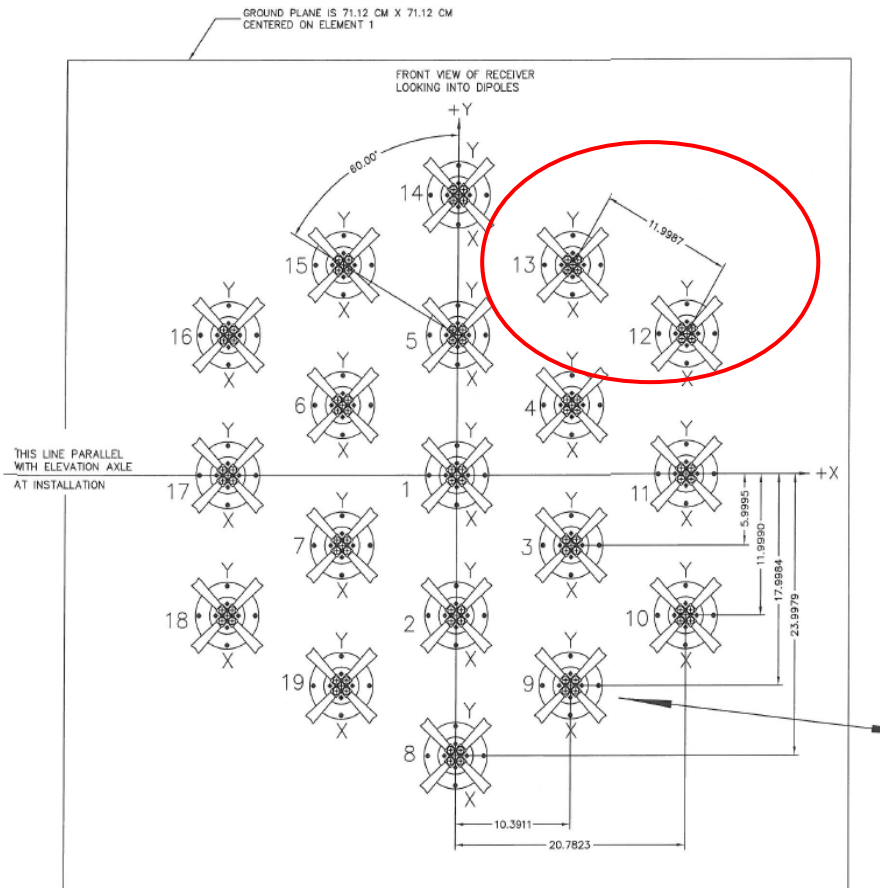
Aperture efficiency – 65 % for $T_{rec} \sim 22$ K

2015: Weights vs offset from boresight



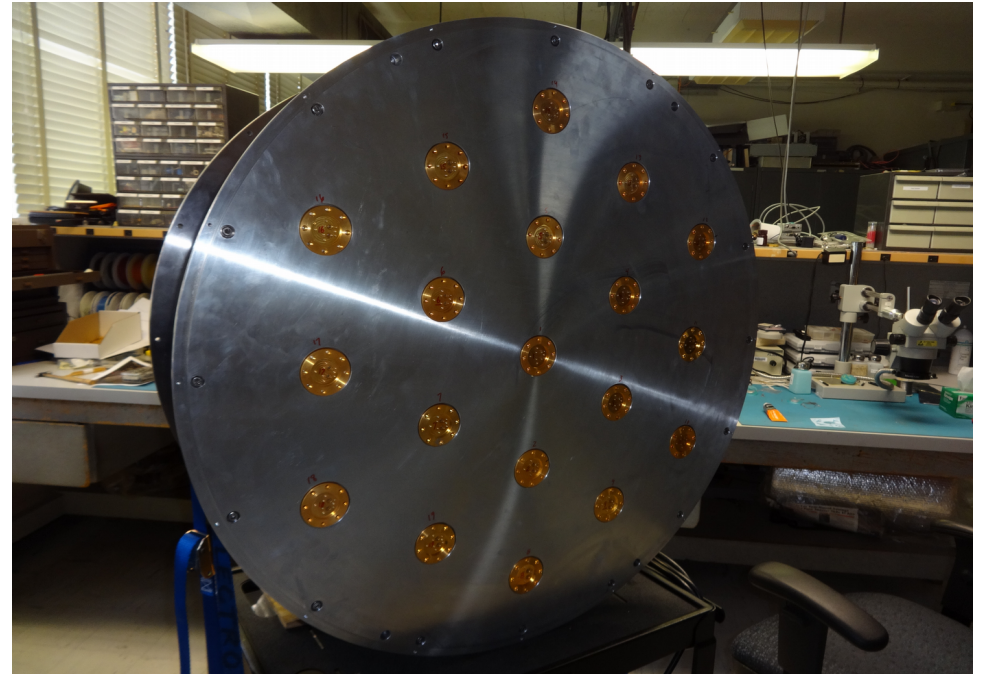
FOV is limited by the array size to ~ 6'

2016: Increase FOV



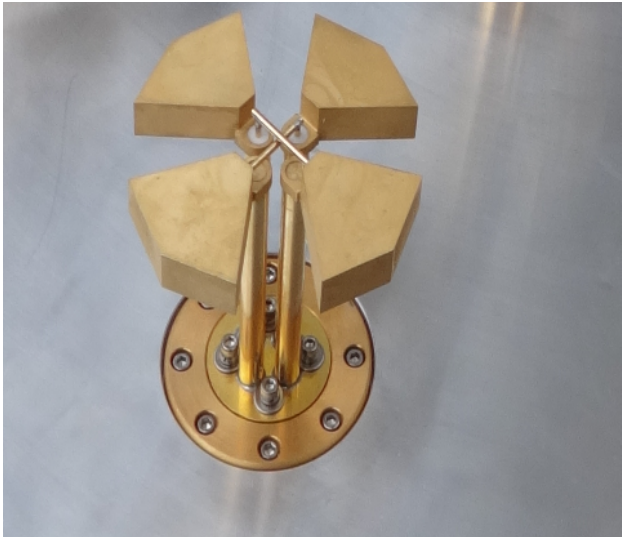
Increase the dipole spacing by ~ 30 %

2016: New Cryo-stat



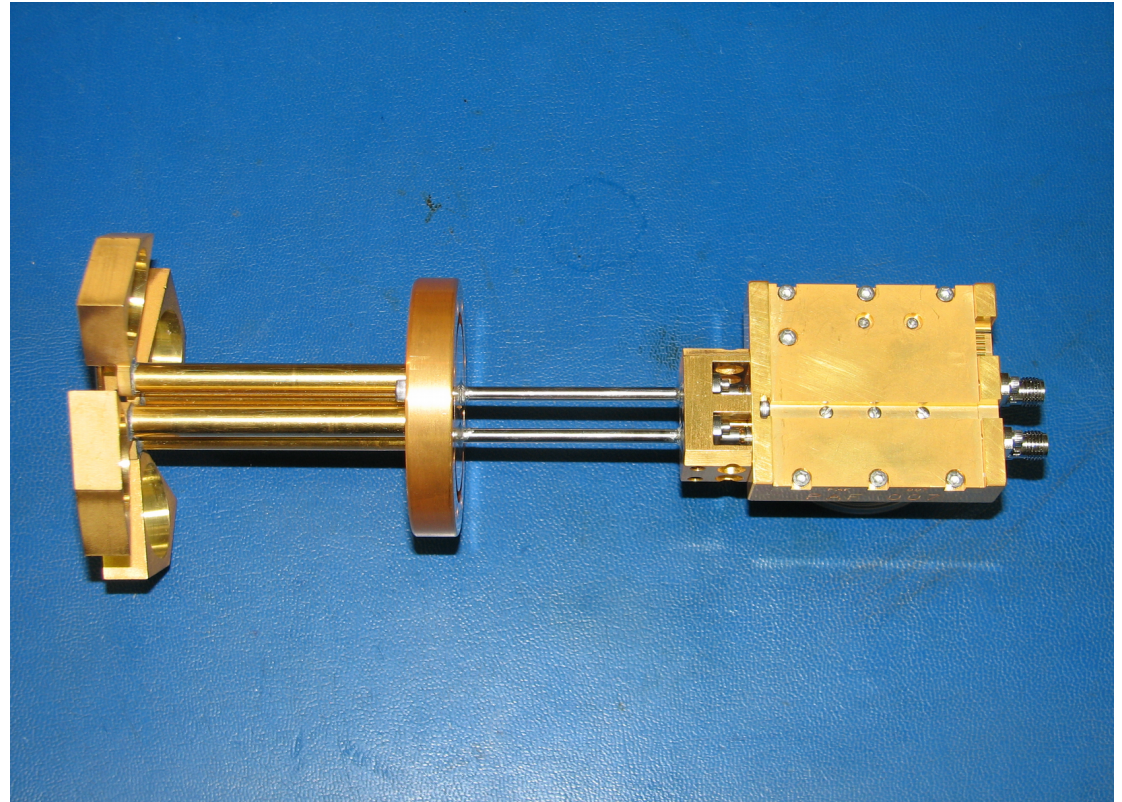
B. Simon, NRAO

2016: New Dipole (GBT2 dipole) and LNA



GBT2 Dipole designed by BYU

Better optimized for the increase
FOV



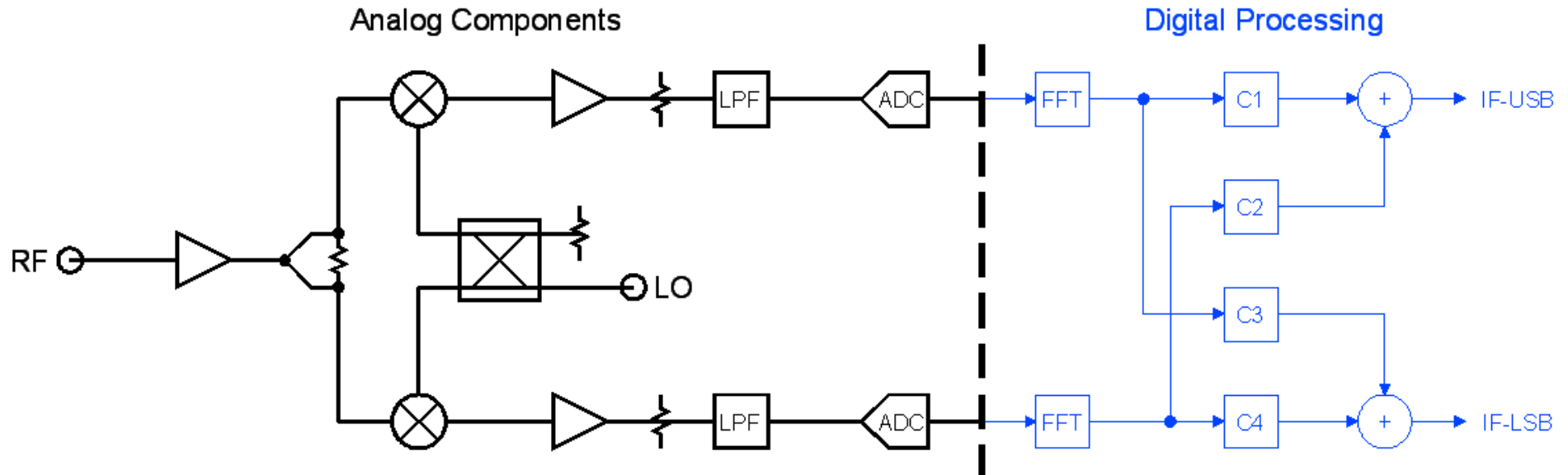
New thermal transition (B. Simon, NRAO)

New amplifiers (W. Groves, Matt, NRAO)
Tamp = 5 K ; (blind mate connectors)

Integrated Unformatted Digital Link

Concept

(Matt & Rick Fisher)



Unformatted: No bit-scrambling, No 8/10 encoding, No packetizing or framing

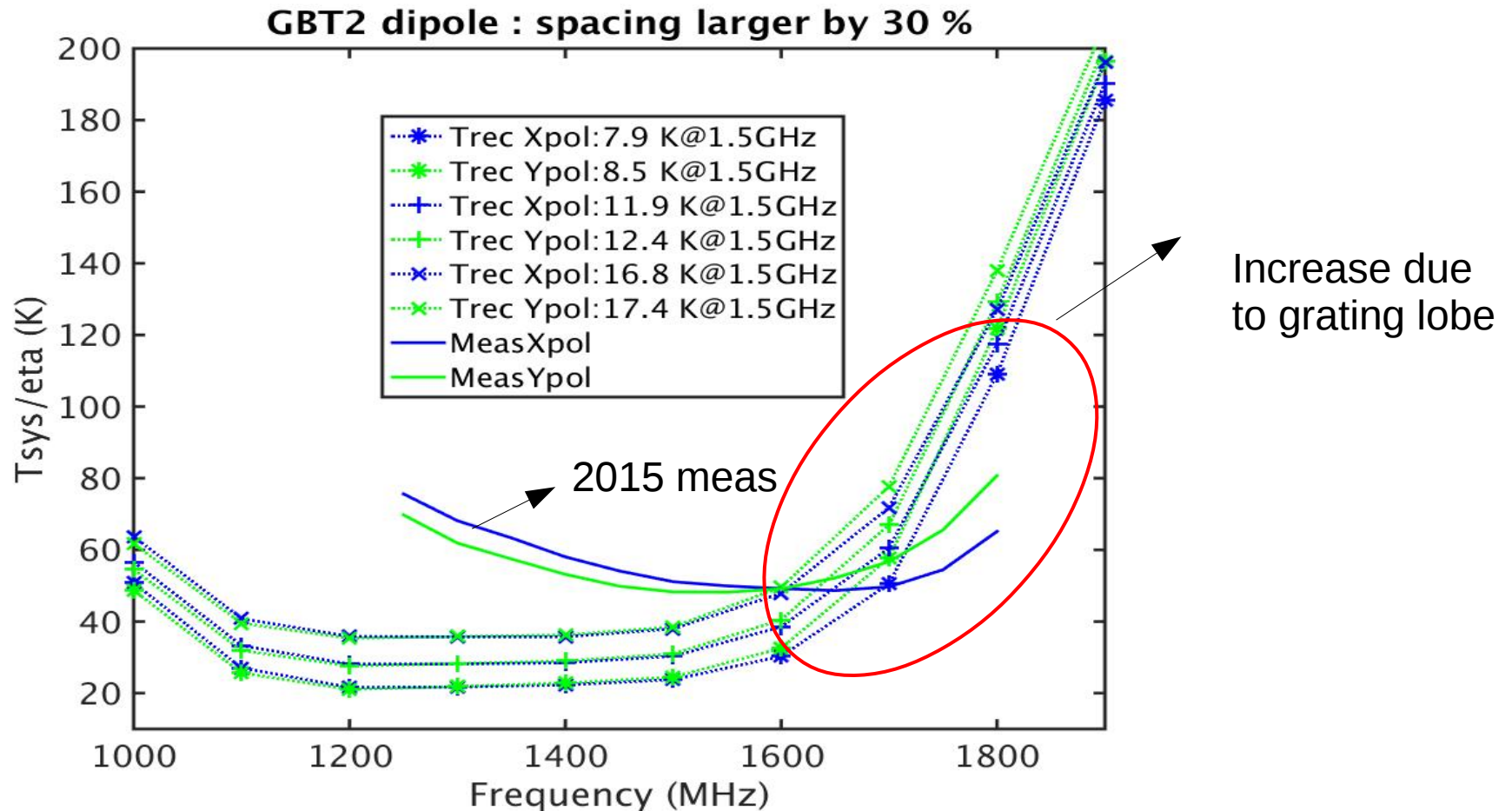
Bandwidth = 150 MHz (Digital downconverter; remove the excess noise from 2015 downconverters)

- M. Morgan and J. Fisher, "Statistical Word Boundary Detection in Serialized Data Streams," U.S. Patent No. 8,688,617, April 1, 2014.
- M. Morgan, J. Fisher, and J. Castro, "Unformatted Digital Fiber-Optic Data Transmission for Radio Astronomy Front Ends," Publications of the Astronomical Society of the Pacific, vol. 125, no. 928, pp. 695-704, June 2013.
- M. Morgan and J. Fisher, "Experiments With Digital Sideband-Separating Downconversion," Publications of the Astronomical Society of the Pacific, vol. 122, no. 889, pp. 326-335, March 2010

PAF Workshop, Aug 24, 2016

2016: NRAO PAF model prediction

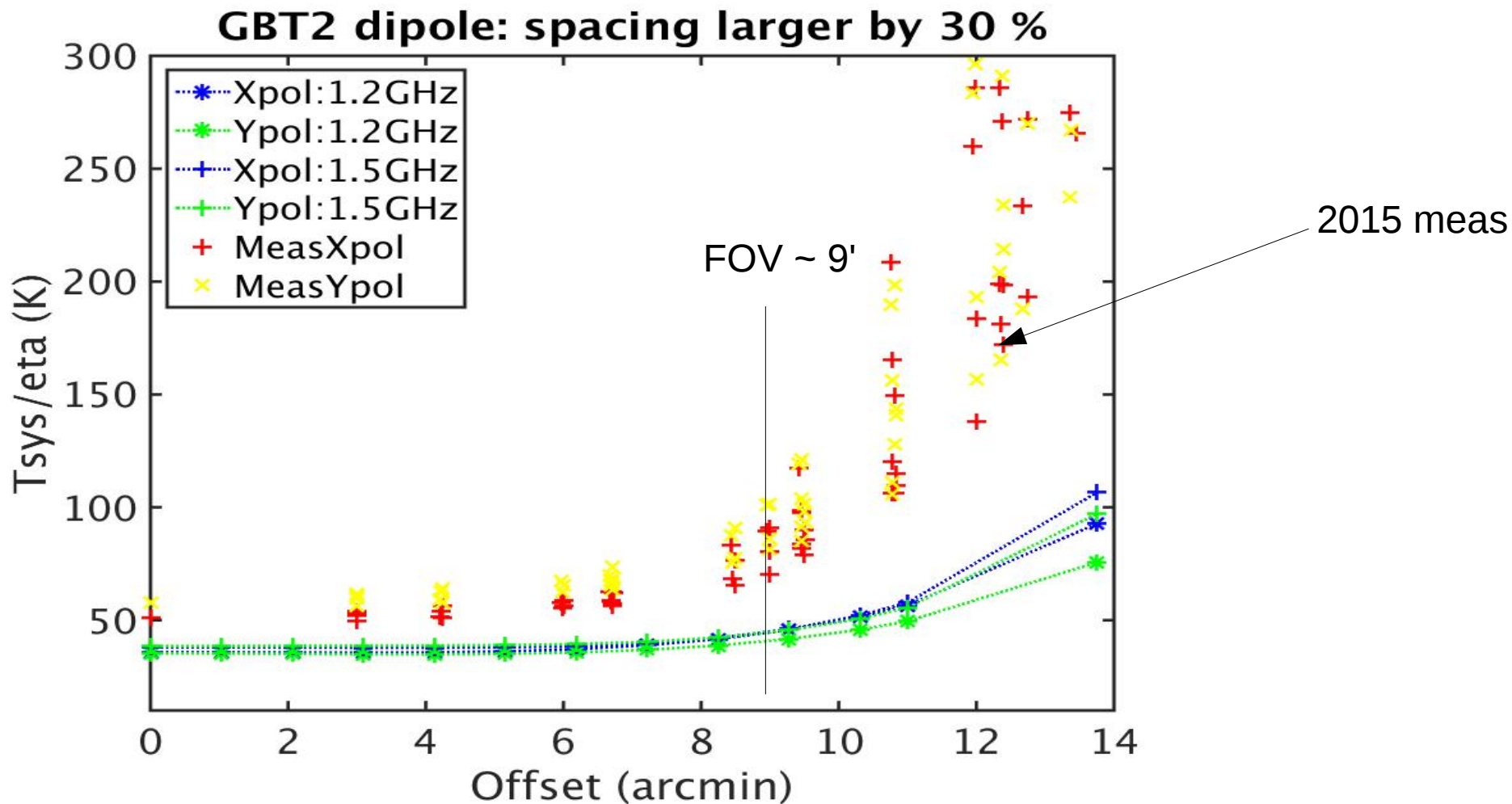
Boresight beam



Expected T_{sys}/η – better than 40 K (depending on the Trec)

2016: NRAO PAF model prediction

Field of View



Expected FOV @ 1.4 GHz – better than 9' ($T_{\text{rec}} \sim 17$ K)

2016 PAF test system and Signal Processing

2015 system



Kite Array

~~Amplifiers
Analog Fiber transmitters~~

~~Analog Fiber receivers
Downconverters~~

~~500 KHz BW
12 bit ADC and voltage recorder~~

Firmware



V. van Tonder
J. Ford et al.
NRAO



GBT2 Array

Cryo LNA

BYU dipoles

Amplifiers
Integrate unformatted
Digital link

ROACH2

Digital Fiber receiver
PFB

1 PFB channel
voltage recorder

ROACH2 hardware
(BYU, WVU grant)

(not BYU beamformer)

$R = \langle VV^H \rangle$

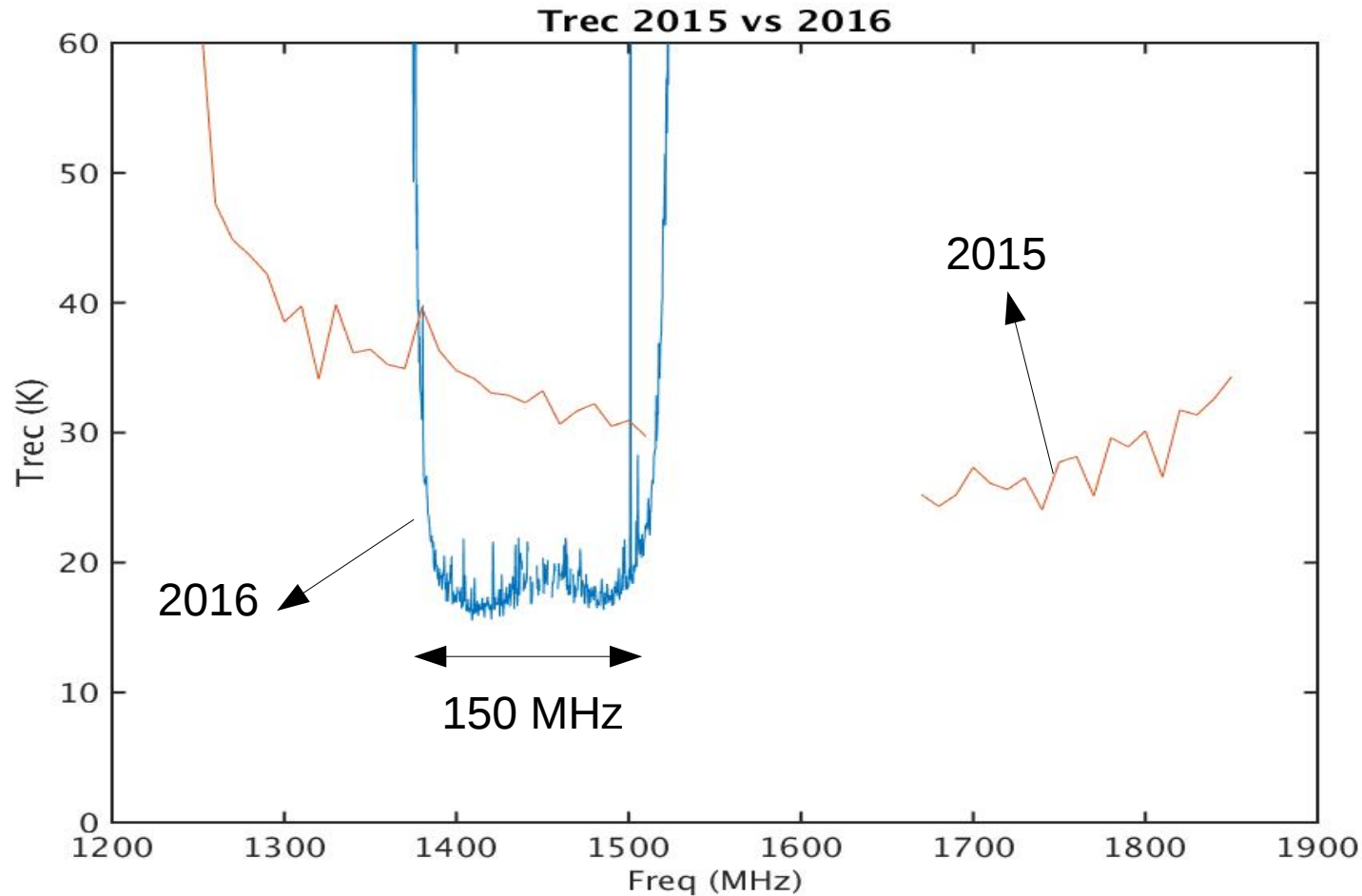
PAF Receiver Temperature Measurement



Outdoor test facility at NRAO, Green Bank

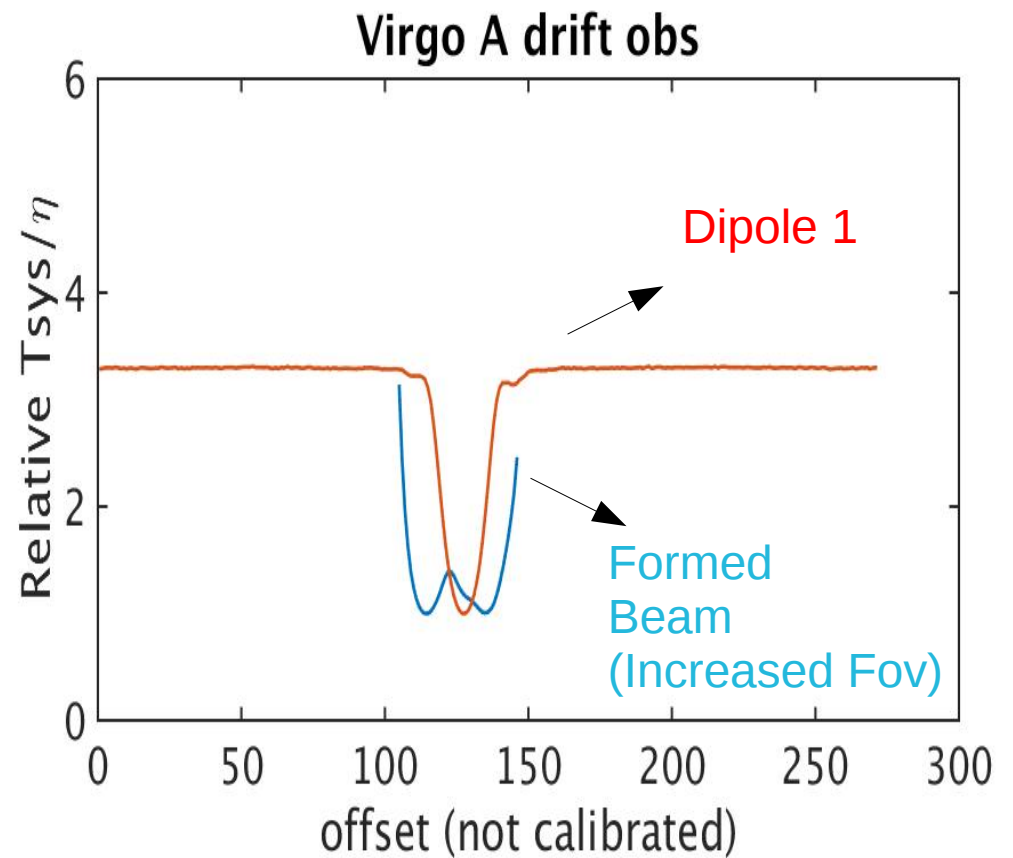
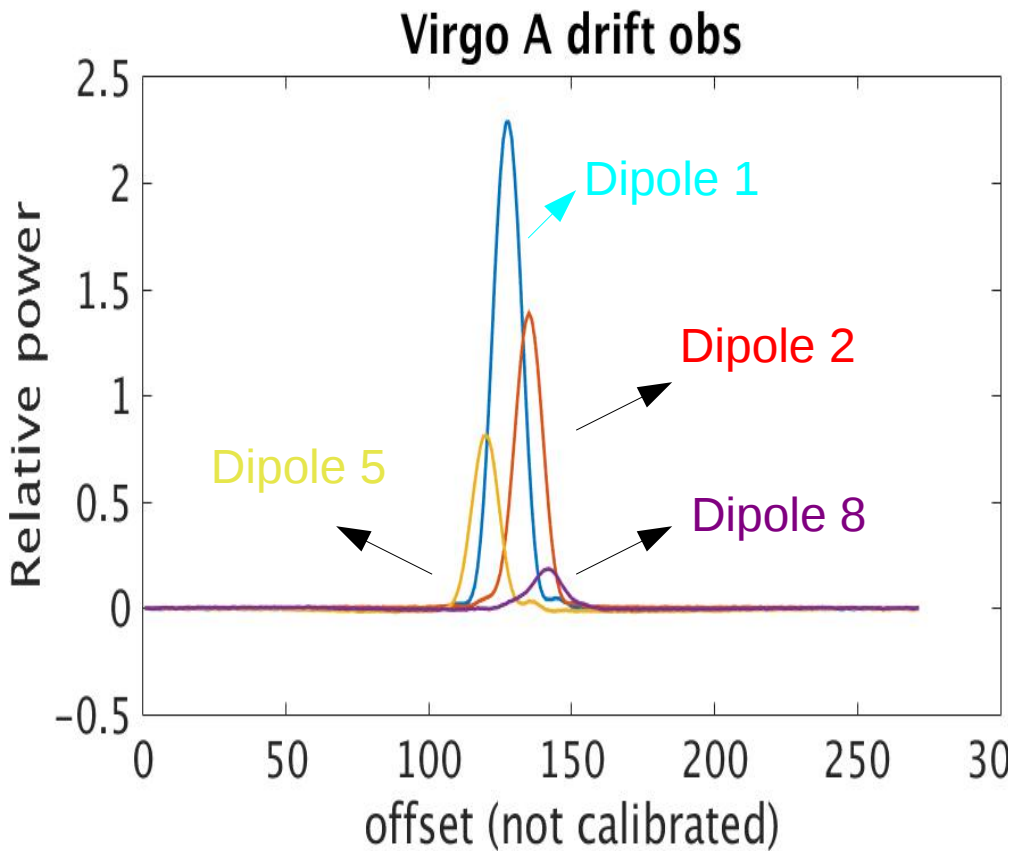
- Hot/Cold voltage correlation measurements → Y factor for a w

2016: PAF Receiver Temperature



- Median Trec (2016; Preliminary result) about 17 K
- 5 to 8 K better than the best trec with replacement transistors + thermal transition of 2015

2016: Virgo A Drift Scan



Need to fix the problem in the new instrument
and redo the measurements

Thank You

Ack: J. D. Nelson, L. Jensen, S. Pan, Bob Dickman.